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2–1. The steel framework is used to support the reinforced stone concrete slab that is used for an office. The slab is 200 mm thick. Sketch the loading that acts along members *BE* and *FED*. Take a = 2 m, b = 5 m. *Hint*: See Tables 1–2 and 1–4.

Beam *BE*. Since $\frac{b}{a} = \frac{5 \text{ m}}{2 \text{ m}} = 2.5$, the concrete slab will behave as a one way slab.

Thus, the tributary area for this beam is rectangular shown in Fig. a and the intensity of the uniform distributed load is

200 mm thick reinforced stone concrete slab: $(23.6 \text{ kN/m}^3)(0.2 \text{ m})(2 \text{ m}) = 9.44 \text{ kN/m}$

Live load for office: $(2.40 \text{ kN/m}^2)(2 \text{ m}) = \frac{480 \text{ kN/m}}{14.24 \text{ kN/m}}$

Due to symmetry the vertical reaction at B and E are

 $B_v = E_v = (14.24 \text{ kN/m})(5)/2 = 35.6 \text{ kN}$

The loading diagram for beam BE is shown in Fig. b.

Beam FED. The only load this beam supports is the vertical reaction of beam BE at E which is $E_y = 35.6$ kN. The loading diagram for this beam is shown in Fig. c.



2–2. Solve Prob. 2–1 with a = 3 m, b = 4 m.

Beam BE. Since $\frac{b}{a} = \frac{4}{3} < 2$, the concrete slab will behave as a two way slab. Thus, the tributary area for this beam is the hexagonal area shown in Fig. *a* and the maximum intensity of the distributed load is

200 mm thick reinforced stone concrete slab: $(23.6 \text{ kN/m}^3)(0.2 \text{ m})(3 \text{ m})$ = 14.16 kN/m

Live load for office:
$$(2.40 \text{ kN/m}^2)(3 \text{ m}) = \frac{720 \text{ kN/m}}{21.36 \text{ kN/m}}$$
 Ans.

Due to symmetry, the vertical reactions at B and E are

$$B_y = E_y = \frac{2\left[\frac{1}{2} (21.36 \text{ kN/m})(1.5 \text{ m})\right] + (21.36 \text{ kN/m})(1 \text{ m})}{2}$$

= 26.70 kN

The loading diagram for Beam *BE* is shown in Fig. *b*.

Beam FED. The loadings that are supported by this beam are the vertical reaction of beam *BE* at *E* which is $E_y = 26.70$ kN and the triangular distributed load of which its tributary area is the triangular area shown in Fig. *a*. Its maximum intensity is

 $= \frac{3.60 \text{ kN/m}}{10.68 \text{ kN/m}}$

200 mm thick reinforced stone concrete slab: $(23.6 \text{ kN/m}^3)(0.2 \text{ m})(1.5 \text{ m})$ = 7.08 kN/m

Live load for office: $(2.40 \text{ kN}/\text{m}^2)(1.5 \text{ m})$





2–3. The floor system used in a school classroom consists of a 4-in. reinforced stone concrete slab. Sketch the loading that acts along the joist *BF* and side girder *ABCDE*. Set a = 10 ft, b = 30 ft. *Hint*: See Tables 1–2 and 1–4.

Joist BF. Since $\frac{b}{a} = \frac{30 \text{ ft}}{10 \text{ ft}} = 3$, the concrete slab will behave as a one way slab. Thus, the tributary area for this joist is the rectangular area shown in Fig. *a* and the intensity of the uniform distributed load is

4 in thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (10 \text{ ft}) = 0.5 \text{ k/ft}$ Live load for classroom: $(0.04 \text{ k/ft}^2)(10 \text{ ft}) = \frac{0.4 \text{ k/ft}}{0.9 \text{ k/ft}}$ Ans.

Due to symmetry, the vertical reactions at B and F are

$$B_y = F_y = (0.9 \text{ k/ft})(30 \text{ ft})/2 = 13.5 \text{ k}$$
 Ans.

The loading diagram for joist BF is shown in Fig. b.

Girder ABCDE. The loads that act on this girder are the vertical reactions of the joists at *B*, *C*, and *D*, which are $B_y = C_y = D_y = 13.5$ k. The loading diagram for this girder is shown in Fig. c.



*2-4. Solve Prob. 2-3 with a = 10 ft, b = 15 ft.

Joist BF. Since $\frac{b}{a} = \frac{15 \text{ ft}}{10 \text{ ft}} = 1.5 < 2$, the concrete slab will behave as a two way slab. Thus, the tributary area for the joist is the hexagonal area as shown in Fig. *a* and the maximum intensity of the distributed load is

4 in thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (10 \text{ ft}) = 0.5 \text{ k/ft}$ Live load for classroom: $(0.04 \text{ k/ft}^2)(10 \text{ ft}) = \frac{0.4 \text{ k/ft}}{0.9 \text{ k/ft}}$ Ans.

Due to symmetry, the vertical reactions at B and G are

$$B_y = F_y = \frac{2\left[\frac{1}{2} (0.9 \text{ k/ft})(5 \text{ ft})\right] + (0.9 \text{ k/ft})(5 \text{ ft})}{2} = 4.50 \text{ k}$$
 Ans.

The loading diagram for beam BF is shown in Fig. b.

Girder ABCDE. The loadings that are supported by this girder are the vertical reactions of the joist at *B*, *C* and *D* which are $B_y = C_y = D_y = 4.50$ k and the triangular distributed load shown in Fig. *a*. Its maximum intensity is

4 in thick reinforced stone concrete slab:

$$(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (5 \text{ ft}) = 0.25 \text{ k/ft}$$

 $= \frac{0.20 \text{ k/ft}}{0.45 \text{ k/ft}}$

Live load for classroom: $(0.04 \text{ k/ft}^2)(5 \text{ ft})$

The loading diagram for the girder ABCDE is shown in Fig. c.





0.9 K/H

2–5. Solve Prob. 2–3 with a = 7.5 ft, b = 20 ft.

Beam BF. Since $\frac{b}{a} = \frac{20 \text{ ft}}{7.5 \text{ ft}} = 2.7 > 2$, the concrete slab will behave as a one way slab. Thus, the tributary area for this beam is a rectangle shown in Fig. *a* and the intensity of the distributed load is

4 in thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (7.5 \text{ ft}) = 0.375 \text{ k/ft}$

Live load from classroom:
$$(0.04 \text{ k/ft}^2)(7.5 \text{ ft}) = \frac{0.300 \text{ k/ft}}{0.675 \text{ k/ft}}$$
 Ans.

Due to symmetry, the vertical reactions at B and F are

$$B_y = F_y = \frac{(0.675 \text{ k/ft})(20 \text{ ft})}{2} = 6.75 \text{ k}$$
 Ans

The loading diagram for beam BF is shown in Fig. b.

Beam ABCD. The loading diagram for this beam is shown in Fig. c.





(८)

2-6. The frame is used to support a 2-in.-thick plywood floor of a residential dwelling. Sketch the loading that acts along members *BG* and *ABCD*. Set a = 5 ft, b = 15 ft. *Hint*: See Tables 1–2 and 1–4.

Beam BG. Since $\frac{b}{a} = \frac{15 \text{ ft}}{5 \text{ ft}} = 3$, the plywood platform will behave as a one way slab. Thus, the tributary area for this beam is rectangular as shown in Fig. *a* and the intensity of the uniform distributed load is

2 in thick plywood platform:
$$\left(36 \frac{\text{lb}}{\text{ft}^2}\right) \left(\frac{2}{12} \text{ ft}\right) (5\text{ft}) = 30 \text{ lb/ft}$$

Line load for residential dweller: $\left(40 \frac{\text{lb}}{\text{ft}^2}\right) (5 \text{ ft}) = \frac{200 \text{ lb/ft}}{230 \text{ lb/ft}}$ Ans

Due to symmetry, the vertical reactions at B and G are

$$B_y = G_y = \frac{(230 \text{ lb/ft})(15 \text{ ft})}{2} = 1725$$
 Ans.

The loading diagram for beam BG is shown in Fig. a.

Beam ABCD. The loads that act on this beam are the vertical reactions of beams BG and CF at B and C which are $B_y = C_y = 1725$ lb. The loading diagram is shown in Fig. c.





D

G

B

Н

Е

2–7. Solve Prob. 2–6, with a = 8 ft, b = 8 ft.

Beam BG. Since $\frac{b}{a} = \frac{8 \text{ ft}}{8 \text{ ft}} = 1 < 2$, the plywood platform will behave as a two way slab. Thus, the tributary area for this beam is the shaded square area shown in Fig. *a* and the maximum intensity of the distributed load is

2 in thick plywood platform: $(36 \text{ lb/ft}^3) \left(\frac{2}{12} \text{ in}\right)(8 \text{ ft}) = 48 \text{ lb/ft}$ Live load for residential dwelling: $(40 \text{ lb/ft})(8 \text{ ft}) = \frac{320 \text{ lb/ft}}{368 \text{ lb/ft}}$

Due to symmetry, the vertical reactions at *B* and *G* are

$$B_y = G_y = \frac{\frac{1}{2}(368 \text{ lb/ft})(8 \text{ ft})}{2} = 736 \text{ lb}$$
 Ans

The loading diagram for the beam BG is shown in Fig. b

Beam *ABCD*. The loadings that are supported by this beam are the vertical reactions of beams *BG* and *CF* at *B* and *C* which are $B_y = C_y = 736$ lb and the distributed load which is the triangular area shown in Fig. *a*. Its maximum intensity is

2 in thick plywood platform: $(36 \text{ lb/ft}^3) \left(\frac{2}{12 \text{ ft}}\right) (4 \text{ ft}) = 24 \text{ lb/ft}$

Live load for residential dwelling: $(40 \text{ lb/ft}^2)(4 \text{ lb/ft}) = \frac{160 \text{ lb/ft}}{184 \text{ lb/ft}}$

The loading diagram for beam *ABCD* is shown in Fig. *c*.





D

368 16/ft

G

B

Ans.

Ans.

Н

E

*2-8. Solve Prob. 2-6, with a = 9 ft, b = 15 ft.

Beam BG. Since $\frac{b}{a} = \frac{15 \text{ ft}}{9 \text{ ft}} = 1.67 < 2$, the plywood platform will behave as a two way slab. Thus, the tributary area for this beam is the octagonal area shown in Fig. *a* and the maximum intensity of the distributed load is

2 in thick plywood platform: $(36 \text{ lb/ft}^3)\left(\frac{2}{12} \text{ in}\right)(9 \text{ ft}) = 54 \text{ lb/ft}$

Live load for residential dwelling: $(40 \text{ lb/ft}^2)(9 \text{ ft}) = \frac{360 \text{ lb/ft}}{414 \text{ lb/ft}}$

Due to symmetry, the vertical reactions at B and G are

$$B_y = G_y = \frac{2\left[\frac{1}{2}(414 \text{ lb/ft})(4.5 \text{ ft})\right] + (414 \text{ lb/ft})(6 \text{ ft})}{2} = 2173.5 \text{ lb}$$

The loading diagram for beam BG is shown in Fig. b.

Beam ABCD. The loading that is supported by this beam are the vertical reactions of beams BG and CF at B and C which is $B_y = C_y = 2173.5$ lb and the triangular distributed load shown in Fig. a. Its maximum intensity is

2 in thick plywood platform: $(36 \text{ lb/ft}^3)\left(\frac{2}{12} \text{ ft}\right)(4.5 \text{ ft}) = 27 \text{ lb/ft}$

Live load for residential dwelling: $(40 \text{ lb/ft}^2)(4.5 \text{ ft}) = \frac{180 \text{ lb/ft}}{207 \text{ lb/ft}}$

The loading diagram for beam *ABCD* is shown in Fig. c.



Ans.

Ans.



D

G

B

Н

Ε

2-9. The steel framework is used to support the 4-in. reinforced stone concrete slab that carries a uniform live loading of 500 lb/ft². Sketch the loading that acts along members *BE* and *FED*. Set b = 10 ft, a = 7.5 ft. *Hint*: See Table 1–2.

Beam BE. Since $\frac{b}{a} = \frac{10}{7.5} < 2$, the concrete slab will behave as a two way slab. Thus, the tributary area for this beam is the octagonal area shown in Fig. *a* and the maximum intensity of the distributed load is

4 in thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (7.5 \text{ ft}) = 0.375 \text{ k/ft}$ Floor Live Load: $(0.5 \text{ k/ft}^2)(7.5 \text{ ft}) = \frac{3.75 \text{ k/ft}}{4.125 \text{ k/ft}}$ Ans.

Due to symmetry, the vertical reactions at *B* and *E* are

$$B_y = E_y = \frac{2\left[\frac{1}{2} (4.125 \text{ k/ft})(3.75 \text{ ft})\right] + (4.125 \text{ k/ft})(2.5 \text{ ft})}{2} = 12.89 \text{ k}$$

The loading diagram for this beam is shown in Fig. b.

Beam FED. The loadings that are supported by this beam are the vertical reaction of beam *BE* at *E* which is $E_y = 12.89$ k and the triangular distributed load shown in Fig. *a*. Its maximum intensity is

4 in thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (3.75 \text{ ft}) = 0.1875 \text{ k/ft}^3$

Floor live load: $(0.5 \text{ k/ft}^2)(3.75 \text{ ft}) = \frac{1.875 \text{ k/ft}}{2.06 \text{ k/ft}}$

The loading diagram for this beam is shown in Fig. c.



4.125 k/ft B 3.75 ft 2.5 ft 3.75 ftBy = 12.89 k (b)



Ans.

2–10. Solve Prob. 2–9, with b = 12 ft, a = 4 ft.

Beam BE. Since $\frac{b}{a} = \frac{12}{4} = 3 > 2$, the concrete slab will behave as a one way slab. Thus, the tributary area for this beam is the rectangular area shown in Fig. *a* and the intensity of the distributed load is 4 in thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^2)\left(\frac{4}{12} \text{ ft}\right)(4 \text{ ft}) = 0.20 \text{ k/ft}$

Floor Live load: $(0.5 \text{ k/ft}^2)(4 \text{ ft}) = \frac{2.00 \text{ k/ft}}{2.20 \text{ k/ft}}$

Due to symmetry, the vertical reactions at B and E are

 $B_y = E_y = \frac{(2.20 \text{ k/ft})(12 \text{ ft})}{2} = 13.2 \text{ k}$

The loading diagram of this beam is shown in Fig. b.

Beam FED. The only load this beam supports is the vertical reaction of beam BE at E which is $E_v = 13.2$ k. Ans.

The loading diagram is shown in Fig. c.



2–11. Classify each of the structures as statically determinate, statically indeterminate, or unstable. If indeterminate, specify the degree of indeterminacy. The supports or connections are to be assumed as stated.





(e) Concurrent reactions Unstable.



Ans.

Ans.

Ans.

Ans.







2-14. Classify each of the structures as statically determinate, statically indeterminate, stable, or unstable. If indeterminate, specify the degree of indeterminacy. The supports or connections are to be assumed as stated.

(a)
$$r = 5$$
 $3n = 3(2) = 6$

r < 3n

Unstable.

(b)
$$r = 9$$
 $3n = 3(3) = 9$

$$r = 3n$$

Stable and statically determinate.

(c)
$$r = 8$$
 $3n = 3(2) = 6$

$$r - 3n = 8 - 6 = 2$$

Stable and statically indeterminate to the second degree.

(a)













2–21. Determine the reactions at the supports *A* and *B* of the compound beam. Assume there is a pin at *C*.



Equations of Equilibrium: First consider the FBD of segment AC in Fig. a. N_A and C_y can be determined directly by writing the moment equations of equilibrium about C and A respectively.

$$\zeta + \sum M_C = 0;$$
 4(6)(3) - N_A(6) = 0 N_A = 12 kN Ans.

$$\zeta + \sum M_A = 0;$$
 $C_y(6) - 4(6)(3) = 0$ $C_y = 12 \text{ kN}$ Ans.

Then,

$$\stackrel{+}{\rightarrow} \sum F_x = 0; \quad 0 - C_x = 0 \qquad C_x = 0$$

Using the FBD of segment *CB*, Fig. *b*,

$$\stackrel{+}{\rightarrow} \sum F_x = 0; \quad 0 + B_x = 0 \qquad \text{Ans.}$$

+
$$\uparrow \sum F_y = 0; \quad B_y - 12 - 18 = 0 \quad B_y = 30 \text{ kN}$$
 Ans.

$$\zeta + \sum M_B = 0;$$
 12(4) + 18(2) - $M_B = 0$ $M_B = 84 \text{ kN} \cdot \text{m}$



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8 k

4 ft 2 ft

 $15 \text{ k} \cdot \text{ft}$

- 8 ft -

8 ft

12 k

2-23. The compound beam is pin supported at C and supported by a roller at A and B. There is a hinge (pin) at D. Determine the reactions at the supports. Neglect the thickness of the beam.

Equations of Equilibrium: Consider the FBD of segment *AD*, Fig. *a*. $\xrightarrow{+} \sum F_x = 0; \quad D_x - 4 \sin 30^\circ = 0 \quad D_x = 2.00 \text{ k}$

 $\zeta + \sum M_D = 0;$ 8(2) + 4 cos 30°(12) - $N_A(6) = 0$ $N_A = 9.59$ k Ans.

$$\zeta + \sum M_A = 0;$$
 $D_y(6) + 4\cos 30^{\circ}(6) - 8(4) = 0$ $D_y = 1.869 \text{ k}$

Now consider the FBD of segment *DBC* shown in Fig. *b*,

$$\stackrel{+}{\longrightarrow} \sum F_x = 0; \quad C_x - 2.00 - 12\left(\frac{3}{5}\right) = 0 \quad C_x = 9.20 \text{ k}$$

$$\zeta + \sum M_C = 0; \quad 1.869(24) + 15 + 12\left(\frac{4}{5}\right)(8) - N_B(16) = 0$$

$$N_B = 8.54 \text{ k}$$
Ans.

$$\zeta + \sum M_B = 0;$$
 1.869(8) + 15 - 12 $\left(\frac{4}{5}\right)$ (8) - $C_y(16) = 0$
 $C_y = 2.93 \text{ k}$ Ans.



*2-24. Determine the reactions on the beam. The support 2 k/ftat *B* can be assumed to be a roller. 12 ft 12 ft **Equations of Equilibrium:** $\zeta + \sum M_A = 0; \quad N_B(24) - 2(12)(6) - \frac{1}{2}(2)(12)(16) = 0 \qquad N_B = 14.0 \text{ k Ans.}$ $\zeta + \sum M_B = 0;$ $\frac{1}{2}(2)(12)(8) + 2(12)(18) - A_y(24) = 0$ $A_y = 22.0$ k Ans. $\stackrel{+}{\rightarrow} \sum F_x = 0; \quad A_x = 0$ Ans. $\frac{1}{z}(z)(12)k$ 2(12)K Aχ 10ft 8ft 6ft Nß Ay (a) 2-25. Determine the reactions at the smooth support C and pinned support A. Assume the connection at B is fixed connected. 80 lb/ft 30°_10 ft 6 ft $\zeta + \sum M_A = 0; \quad C_y (10 + 6 \sin 60^\circ) - 480(3) = 0$ $C_y = 94.76 \text{ lb} = 94.8 \text{ lb}$ $\xrightarrow{+} \sum F_x = 0; \quad A_x - 94.76 \sin 30^\circ = 0$ Ans. 48016 $A_v = 47.4 \, \text{lb}$ Ans. 30 $+\uparrow \sum F_y = 0; A_y + 94.76 \cos 30^\circ - 480 = 0$ 10' 31 $A_{y} = 398 \, \text{lb}$ Ans.

0

2–26. Determine the reactions at the truss supports *A* and *B*. The distributed loading is caused by wind.



$$\zeta + \sum M_A = 0; \quad B_y(96) + \left(\frac{12}{13}\right) 20.8(72) - \left(\frac{5}{13}\right) 20.8(10) - \left(\frac{12}{13}\right) 31.2(24) - \left(\frac{5}{13}\right) 31.2(10) =$$

$$+\uparrow \sum F_y = 0; \quad A_y - 5.117 + \left(\frac{12}{13}\right) 20.8 - \left(\frac{12}{13}\right) 31.2 = 0$$

 $A_y = 14.7 \text{ kN}$

Ans.

Ans.

$$\stackrel{+}{\longrightarrow} \sum F_x = 0; \quad -B_x + \left(\frac{5}{13}\right) 31.2 + \left(\frac{5}{13}\right) 20.8 = 0$$

 $B_x = 20.0 \text{ kN}$

 $B_{y} = 5.117 \text{ kN} = 5.12 \text{ kN}$





*2–28. Determine the reactions at the supports A and B. The floor decks CD, DE, EF, and FG transmit their loads to the girder on smooth supports. Assume A is a roller and B is a pin.

Consider the entire system.

$$\zeta + \sum M_B = 0; \quad 10(1) + 12(10) - A_y (8) = 0$$
$$A_y = 16.25 \text{ k} = 16.3 \text{ k}$$
$$\stackrel{+}{\rightarrow} \sum F_x = 0; \quad B_x = 0$$
$$+ \uparrow \sum F_y = 0; \quad 16.25 - 12 - 10 + B_y = 0$$
$$B_y = 5.75 \text{ k}$$



2–29. Determine the reactions at the supports *A* and *B* of the compound beam. There is a pin at *C*.

Member AC:

 $\zeta + \sum M_C = 0; -A_y(6) + 12(2) = 0$ $A_y = 4.00 \text{ kN}$ $+ \uparrow \sum F_y = 0; \quad C_y + 4.00 - 12 = 0$ $C_y = 8.00 \text{ kN}$ $\stackrel{+}{\rightarrow} \sum F_x = 0; \quad C_x = 0$ Member CB: $\zeta + \sum M_B = 0; -M_B + 8.00(4.5) + 9(3) = 0$ $M_B = 63.0 \text{ kN} \cdot \text{m}$ $+ \uparrow \sum F_y = 0; \quad B_y - 8 - 9 = 0$ $B_y = 17.0 \text{ kN}$ $\stackrel{+}{\rightarrow} \sum F_x = 0; \quad B_x = 0$







2–31. The beam is subjected to the two concentrated loads as shown. Assuming that the foundation exerts a linearly varying load distribution on its bottom, determine the load intensities w_1 and w_2 for equilibrium (a) in terms of the parameters shown; (b) set P = 500 lb, L = 12 ft.



Equations of Equilibrium: The load intensity w_1 can be determined directly by summing moments about point A.

$$\zeta + \sum M_A = 0; \quad P\left(\frac{L}{3}\right) - w_1 L\left(\frac{L}{6}\right) = 0$$

$$w_1 = \frac{2P}{L}$$

$$+ \uparrow \sum F_y = 0; \quad \frac{1}{2} \left(w_2 - \frac{2P}{L}\right)L + \frac{2P}{L}(L) - 3P = 0$$

$$w_2 = \left(\frac{4P}{L}\right)$$
Ans

If P = 500 lb and L = 12 ft,

$$w_1 = \frac{2(500)}{12} = 83.3 \, \text{lb/ft}$$
 Ans.

$$w_2 = \frac{4(500)}{12} = 167 \, \text{lb/ft}$$
 Ans.



20 000 lb *2-32 The cantilever footing is used to support a wall near its edge A so that it causes a uniform soil pressure under the 8000 lb footing. Determine the uniform distribution loads, w_A and 0.25 ft w_B , measured in lb/ft at pads A and B, necessary to support the wall forces of 8000 lb and 20 000 lb. 1.5 ft R A w_B -2 ft $8 \, {\rm ft}$ -3 ft- $\zeta + \sum M_A = 0;$ -8000(10.5) + $w_B(3)(10.5) + 20\,000(0.75) = 0$ $w_B = 2190.5 \text{ lb/ft} = 2.19 \text{ k/ft}$ Ans. $+\uparrow \sum F_y = 0;$ 2190.5(3) - 28 000 + w_A (2) = 0 20.000) 8,00016 1.5代 $w_A = 10.7 \text{ k/ft}$ Ans. 0.25 F 10.5 Ft 2-33. Determine the horizontal and vertical components В of reaction acting at the supports A and C. 2 m 4'm 30 kN 2 m 50 kN 4 m 3 m -- 3 m 1.5 m 1.5 m Equations of Equilibrium: Referring to the FBDs of segments AB and BC respectively shown in Fig. a, $\zeta + \sum M_A = 0; \quad B_x(8) + B_y(6) - 50(4) = 0$ (1) $\zeta + \sum M_C = 0; \quad B_v(3) - B_x(4) + 30(2) = 0$ By (2)6m 3m Bx Bχ 2m 30KN-4m гm .50 KN 4m (a)

2-33. Continued Solving, $B_y = 6.667 \text{ kN}$ $B_x = 20.0 \text{ kN}$ Segment *AB*, $\stackrel{+}{\longrightarrow} \sum F_x = 0;$ 50 - 20.0 - $A_x = 0$ $A_x = 30.0$ kN Ans. $+\uparrow \sum F_y = 0;$ 6.667 - $A_y = 0$ $A_y = 6.67$ kN Ans. Segment BC, $\stackrel{+}{\longrightarrow} \sum F_x = 0; \quad C_x + 20.0 - 30 = 0 \quad C_x - 10.0 \text{ kN}$ Ans. $+\uparrow \sum F_y = 0;$ $C_y - 6.667 = 0$ Cy = 6.67 kN Ans. 2-34. Determine the reactions at the smooth support A 150 lb/ft and the pin support B. The joint at C is fixed connected. -10 ft -5 ft Equations of Equilibrium: Referring to the FBD in Fig. a. $\zeta + \sum M_B = 0;$ $N_A \cos 60^{\circ}(10) - N_A \sin 60^{\circ}(5) - 150(10)(5) = 0$ $N_A = 11196.15 \text{ lb} = 11.2 \text{ k}$ Ans. $\stackrel{+}{\to} \sum F_x = 0; \qquad B_x - 11196.15 \sin 60^\circ = 0$ $B_x = 9696.15 \text{ lb} = 9.70 \text{ k}$ Ans. $+\uparrow \sum F_y = 0;$ 11196.15 cos 60° - 150(10) - $B_y = 0$ Ans. $B_v = 4098.08 \, \text{lb} = 4.10 \, \text{k}$ 150(10)1b 5ft 51 B_x 5ft Вų 60° NA

39

(a)



Ans.

2–37. Determine the horizontal and vertical components force at pins A and C of the two-member frame.



Free Body Diagram: The solution for this problem will be simplified if one realizes that member BC is a two force member.

Equations of Equilibrium:

$$\zeta + \sum M_A = 0;$$
 $F_{BC} \cos 45^{\circ} (3) - 600 (1.5) = 0$
 $F_{BC} = 424.26 \text{ N}$

$$+\uparrow \sum F_y = 0;$$
 $A_y + 424.26\cos 45^\circ - 600 = 0$

$$A_y = 300 \text{ N}$$

$$\stackrel{+}{\to} \sum F_x = 0;$$
 424.26 sin 45° - $A_x = 0$ Ans.

 $A_x = 300 \text{ N}$

For pin *C*,

$$C_x = F_{BC} \sin 45^\circ = 424.26 \sin 45^\circ = 300 \text{ N}$$
 Ans.
 $C_y = F_{BC} \cos 45^\circ = 424.26 \cos 45^\circ = 300 \text{ N}$ Ans.

$$C_y = F_{BC} \cos 45^\circ = 424.26 \cos 45^\circ = 300 \text{ N}$$



2–38. The wall crane supports a load of 700 lb. Determine the horizontal and vertical components of reaction at the pins A and D. Also, what is the force in the cable at the winch W?

Pulley E:

$$+\uparrow \Sigma F_y = 0; \quad 2T - 700 = 0$$
$$T = 350 \text{ lb}$$

Member *ABC*:

 $\zeta + \sum M_A = 0;$ $T_{BD} \sin 45^{\circ} (4) - 350 \sin 60^{\circ} (4) - 700(8) = 0$ $T_{BD} = 2409 \text{ lb}$

$$+\uparrow \sum F_y = 0;$$
 $A_y + 2409 \sin 45^\circ - 350 \sin 60^\circ - 700 = 0$

 $A_y = 700 \, \text{lb}$

 $\stackrel{+}{\longrightarrow} \sum F_x = 0; \qquad A_x - 2409 \cos 45^\circ - 350 \cos 60^\circ + 350 - 350 = 0$

$$A_x = 1.88 \,\mathrm{k}$$

At D:

$$D_x = 2409 \cos 45^\circ = 1703.1 \, \text{lb} = 1.70 \, \text{k}$$

 $D_y = 2409 \sin 45^\circ = 1.70 \text{ k}$



2–39. Determine the resultant forces at pins *B* and *C* on member *ABC* of the four-member frame.

$$\zeta + \sum M_F = 0; \quad F_{CD}(7) - \frac{4}{5} F_{BE}(2) = 0$$

$$\zeta + \sum M_A = 0; \quad -150(7)(3.5) + \frac{4}{5} F_{BE}(5) - F_{CD}(7) = 0$$

$$F_{BE} = 1531 \text{ lb} = 1.53 \text{ k} \qquad \text{Ans.}$$

$$F_{CD} = 350 \text{ lb} \qquad \text{Ans.}$$





*2–40. Determine the reactions at the supports is *A* and *D*. Assume *A* is fixed and *B* and *C* and *D* are pins.

Member *BC*:

$$\zeta + \sum M_B = 0; \quad C_y (1.5L) - (1.5wL) \left(\frac{1.5L}{2}\right) = 0$$

 $C_y = 0.75 wL$

$$+\uparrow \sum F_y = 0; B_y - 1.5wL + 0.75wL = 0$$

 $B_y = 0.75wL$

Member CD:

$$\zeta + \sum M_D = 0; \quad C_x = 0$$

$$\stackrel{+}{\rightarrow} \sum F_x = 0; \quad D_x = 0$$

$$+ \uparrow \sum F_y = 0; \quad D_y - 0.75wL = 0$$

$$D_y = 0.75 wL$$



Ans. Ans.

Ans.

Ans.

*2-40. Continued

Member BC: $\stackrel{+}{\rightarrow} \sum F_x = 0; \quad B_x - 0 = 0; \quad B_x = 0$ Member AB: $\stackrel{+}{\rightarrow} \sum F_x = 0; \quad wL - A_x = 0$ $A_x = wL$ $+ \uparrow \sum F_y = 0; \quad A_y - 0.75 \ wL = 0$ $A_y = 0.75 \ wL$ $\zeta + \sum M_A = 0; \quad M_A - wL \left(\frac{L}{2}\right) = 0$ $M_A = \frac{wL^2}{2}$



2-41. Determine the horizontal and vertical reactions at the connections A and C of the gable frame. Assume that A, B, and C are pin connections. The purlin loads such as D and E are applied perpendicular to the center line of each girder.



Member *AB*:

$$\zeta + \sum M_A = 0; \quad B_x(15) + B_y(12) - (1200)(5) - 600 \left(\frac{12}{13}\right)(16) - 600 \left(\frac{5}{13}\right)(12.5) - 400 \left(\frac{12}{13}\right)(12) - 400 \left(\frac{5}{13}\right)(15) = 0 B_x(15) + B_y(12) = 18,946.154$$
(1)

Member BC:

$$\zeta + \sum M_C = 0; \quad -(B_x)(15) + B_y(12) + (600) \left(\frac{12}{13}\right)(6) + 600 \left(\frac{5}{13}\right)(12.5) + 400 \left(\frac{12}{13}\right)(12) + 400 \left(\frac{5}{13}\right)(15) = 0 B_x(15) - B_y(12) = 12.946.15$$
(2)



Ans.

2-41. Continued

Solving Eqs. (1) and (2),

$$B_x = 1063.08 \, \text{lb}, \qquad B_y = 250.0 \, \text{lb}$$

Member *AB*:

$$\xrightarrow{+} \sum F_x = 0; \quad -A_x + 1200 + 1000 \left(\frac{5}{13}\right) - 1063.08 = 0$$

$$A_x = 522 \text{ lb}$$

$$+\uparrow \sum F_y = 0;$$
 $A_y - 800 - 1000 \left(\frac{12}{13}\right) + 250 = 0$

$$A_y = 1473 \, \text{lb} = 1.47 \, \text{k}$$
 Ans

Member BC:

$$\stackrel{+}{\rightarrow} \sum F_x = 0; \quad -C_x - 1000 \left(\frac{5}{13}\right) + 1063.08 = 0$$

$$C_x = 678 \text{ lb} \qquad \text{Ans.}$$

$$+ \uparrow \sum F_y = 0; \qquad C_y - 800 - 1000 \left(\frac{12}{13}\right) + 250.0 = 0$$

$$C_y = 1973 \text{ lb} = 1.97 \text{ k} \qquad \text{Ans.}$$

2-42. Determine the horizontal and vertical components of reaction at A, C, and D. Assume the frame is pin connected at A, C, and D, and there is a fixed-connected joint at B.





2–42. Continued $+\uparrow \sum F_y = 0;$ $A_y + 7.00 - 50 - 40 = 0$ $A_y = 83.0 \, \text{kN}$ Ans. $\stackrel{+}{\rightarrow} \sum F_x = 0; \qquad A_x - 45.0 = 0$ $A_{\rm x} = 45.0 \, \rm kN$ Ans. From Eq. (1). $D_y = 7.00 \text{ kN}$ Ans. 2-43. Determine the horizontal and vertical components k/ft at A, B, and C. Assume the frame is pin connected at these points. The joints at D and E are fixed connected. 6 ft 1.5 k/ft 10 ft -18 ft – —18 ft - $\zeta + \sum M_A = 0;$ -18 ft $(B_v) + 16$ ft $(B_x) = 0$ (1) $\zeta + \sum M_C = 0; 15 \text{ k} (5\text{ft}) + 9 \text{ ft} (56.92 \text{ k} (\cos 18.43^\circ)) + 13 \text{ ft} (56.92 \text{ k} (\sin 18.43^\circ))$ $-16 \text{ ft} (B_x) - 18 \text{ ft} (B_x) = 0$ (2)Solving Eq. 1 & 2 $B_x = 24.84 \text{ k}$ Ans. $B_y = 22.08 \,\mathrm{k}$ Ans. $\xrightarrow{+} \sum F_x = 0; \quad A_x - 24.84 \, \mathrm{k} = 0$ $A_x = 24.84 \text{ k}$ $+\uparrow \sum F_{y} = 0; A_{y} - 22.08 k = 0$ $A_v = 22.08 \,\mathrm{k}$ $\stackrel{+}{\rightarrow} \sum F_x = 0; \quad C_x - 15 \text{ k} - \sin(18.43^\circ) (56.92 \text{ k}) + 24.84 \text{ k}$ $C_x = 8.16 \,\mathrm{k}$ Ans. $+\uparrow \sum F_y = 0; \quad Cy + 22.08 \text{ k} - \cos(18.43^\circ)(56.92 \text{ k}) = 0$ Cy = 31.9 kAns. 56.92 k B 64 18.43 131 24 × L 10ft 15 k Ay 18A

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